

## ZERO BRINE Project Meeting – WP5

June 21th, Athens

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NTUA, UNIPA, TUDELFT, CTM,



Knowledge for Tomorrow

## 5.1 - Refurbishment and minor design modifications (upgrade) of pilot brine treatment systems

Technology	Current Activities	Planned finalization
<b>MED</b>	<ul style="list-style-type: none"><li>- Refurbished and fully installed on the Greek BEC</li><li>- Ready for upcoming experiments on the UEST Lab</li></ul>	M18
<b>EFC</b>	<ul style="list-style-type: none"><li>- Ready for shipping to WP4</li></ul>	M18
<b>Crystallizer</b>	<ul style="list-style-type: none"><li>- Lab scale: Multiple Feed – Plug Flow Reactor (MF-PFR), CSTR, CrIEM</li><li>- Pilot unit: MF-PFR for recovery of Mg &amp; Ca</li><li>- Ready for shipping to WP2</li></ul>	M18



## 5.1 - Refurbishment and minor design modifications (upgrade) of pilot brine treatment systems



**MED**



**EFC**



**Crystallizer**

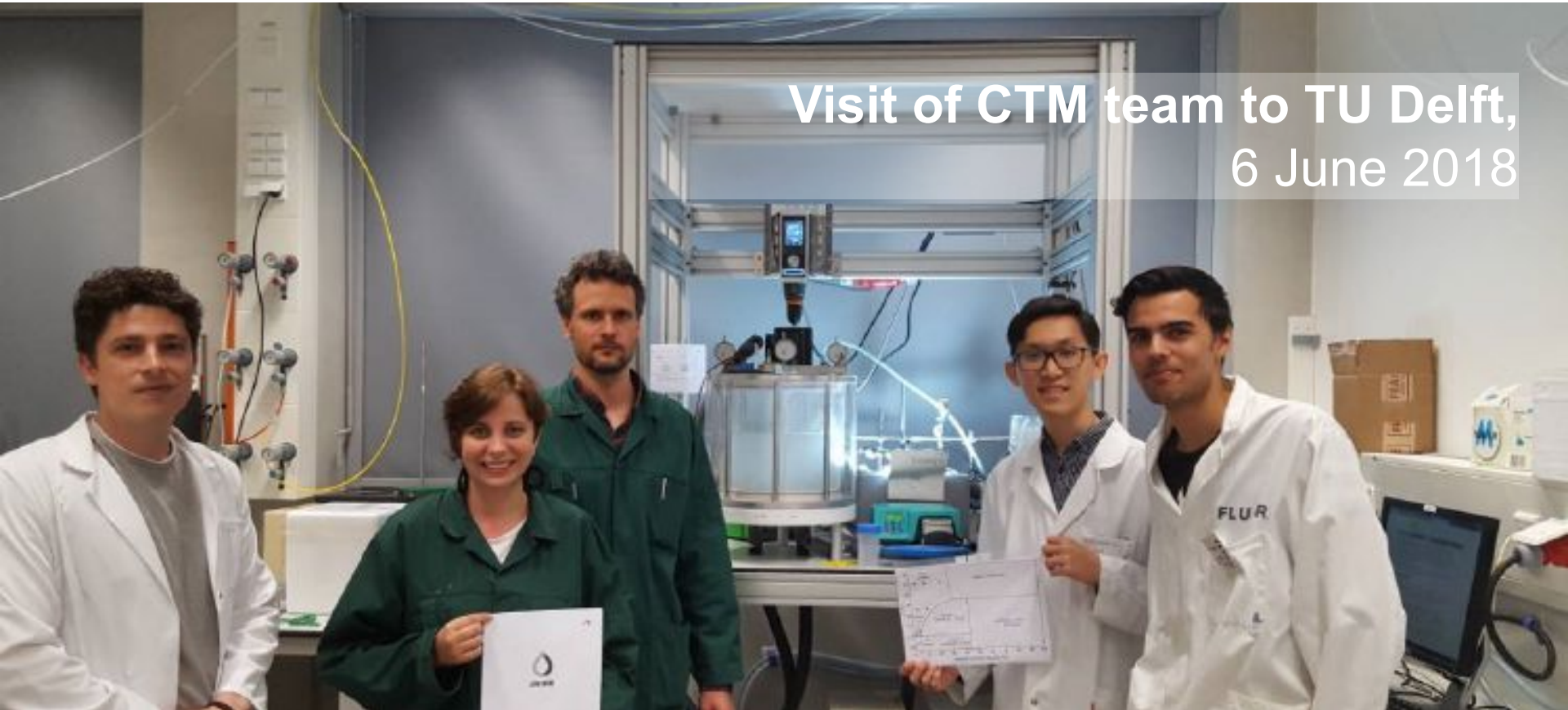


## 5.2 - BECs



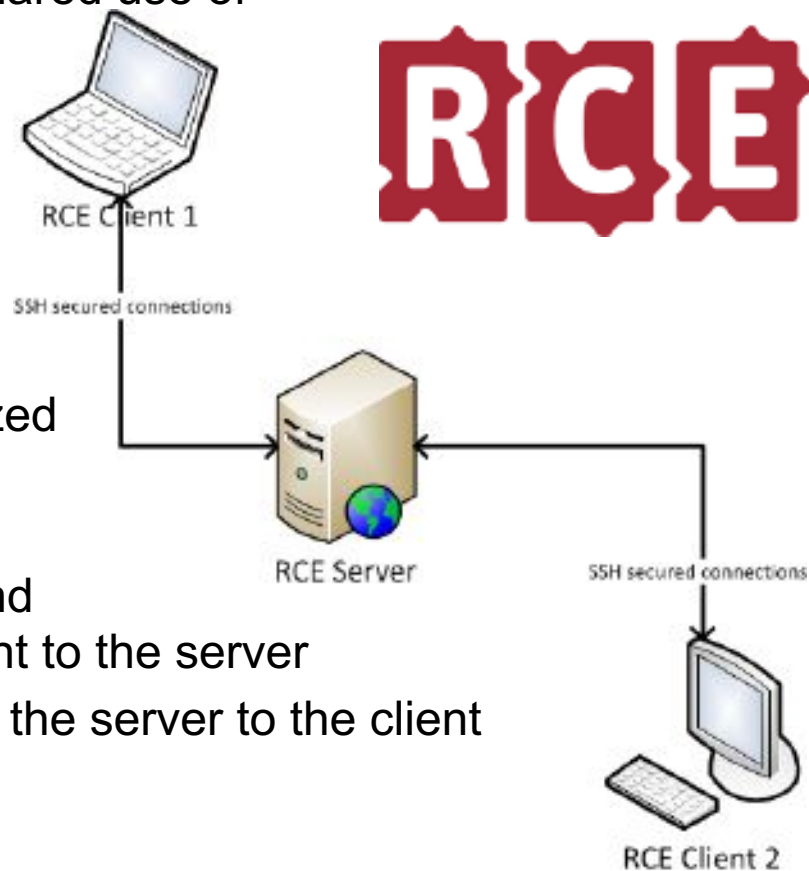


## Subtask 5.2.2: Plans for shared use of BEC equipment



## 5.3 – Development of technology libraries (software tool) and integration into a common platform

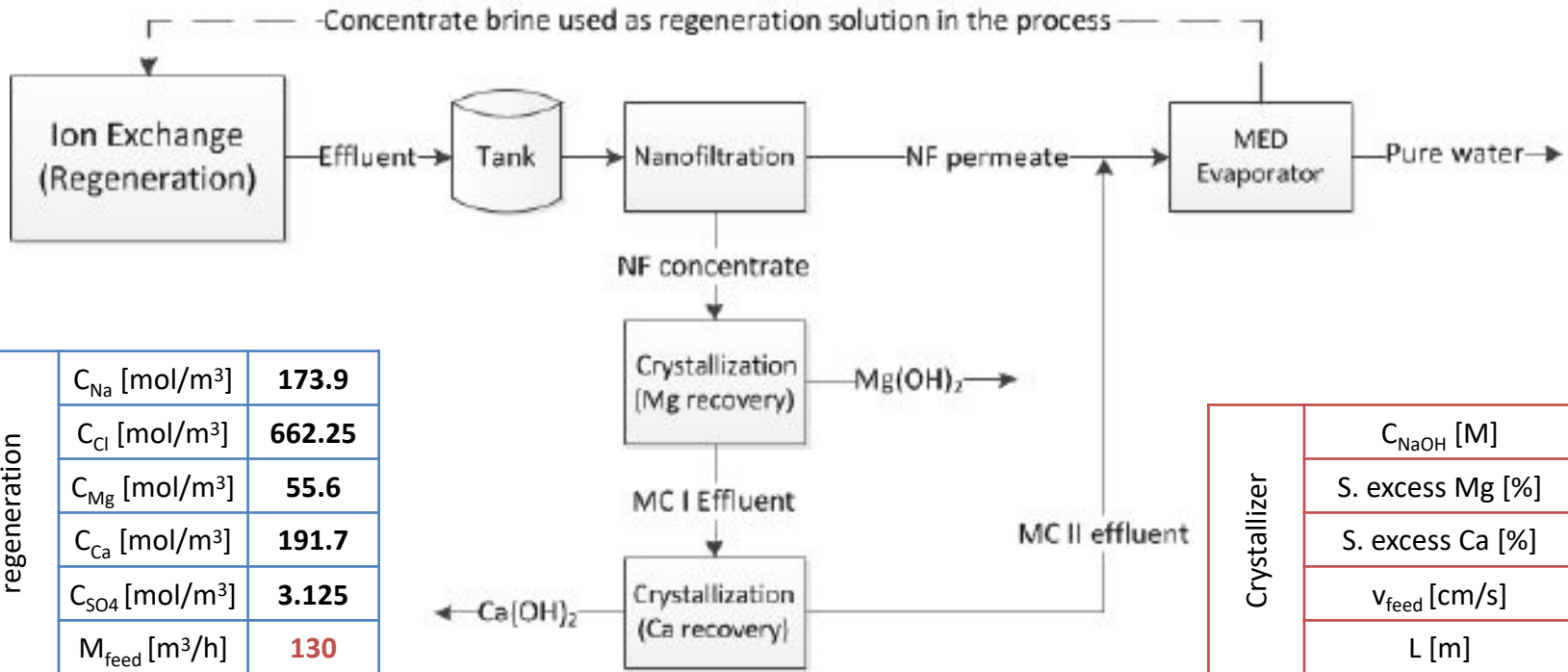
- Java framework by DLR for remote and shared use of models/simulations
- Simulations are defined as workflows which consist of linked modules
- Environment consists of a server and one or more clients
- Simulation code has to be installed on the RCE Server and can be run by all authorized clients
- Configuration of simulations and required input data can be provided by the client and are automatically transferred from the client to the server
- Results are automatically transferred from the server to the client



Model	Responsible	Main Features	Status
<b>MED</b>	DLR/Python	<ul style="list-style-type: none"> <li>- Forward-feed and parallel-cross feed arrangement</li> <li>- CAPEX (Module Costing Technique) and OPEX estimation</li> </ul>	10/17
<b>RO</b>	DLR/Python	<ul style="list-style-type: none"> <li>- Single stage or permeate staging arrangement</li> <li>- varying <math>P_{\text{feed}}</math> and <math>n_{\text{stages}}</math> for a required R (cost min)</li> </ul>	02/18
<b>NF</b>	DLR/Python	<ul style="list-style-type: none"> <li>- Batch and plug flow reactor</li> <li>- Economic estimations based on overall mass balances</li> </ul>	current
<b>Cryst.</b>	DLR/Python	<ul style="list-style-type: none"> <li>- Hierarchical model: from membrane to plant scale</li> <li>- CAPEX and OPEX</li> </ul>	04/18
<b>MD</b>	DLR/Python	-	pending
<b>IEX</b>	DLR/Python	-	pending
<b>EFC</b>	CTM/Matlab	<ul style="list-style-type: none"> <li>- Data Driven approach: bench scale monitoring results</li> <li>- Theoretical energy model: stochastic, thermodynamic</li> <li>- Link to energy supply unit (NH<sub>3</sub>-H<sub>2</sub>O absorption chiller)-EFC</li> </ul>	current
<b>ED</b>	CTM/Matlab	<ul style="list-style-type: none"> <li>- Data Driven approach: bench scale monitoring results</li> <li>- Theoretical energy modelisation: lumped modeling</li> </ul>	pending



# First treatment chain: EVIDES Site I



Effluent from the IEX regeneration	$C_{Na}$ [mol/m <sup>3</sup> ]	<b>173.9</b>
	$C_{Cl}$ [mol/m <sup>3</sup> ]	<b>662.25</b>
	$C_{Mg}$ [mol/m <sup>3</sup> ]	<b>55.6</b>
	$C_{Ca}$ [mol/m <sup>3</sup> ]	<b>191.7</b>
	$C_{SO4}$ [mol/m <sup>3</sup> ]	<b>3.125</b>
	$M_{feed}$ [m <sup>3</sup> /h]	<b>130</b>
NF membrane properties	$r_{pore}$ [nm]	0.45
	$\delta_m$ [μm]	3
	$\epsilon_{pore}$ [-]	56.5
	$X_d$ [mol/m <sup>3</sup> ]	<b>40</b>

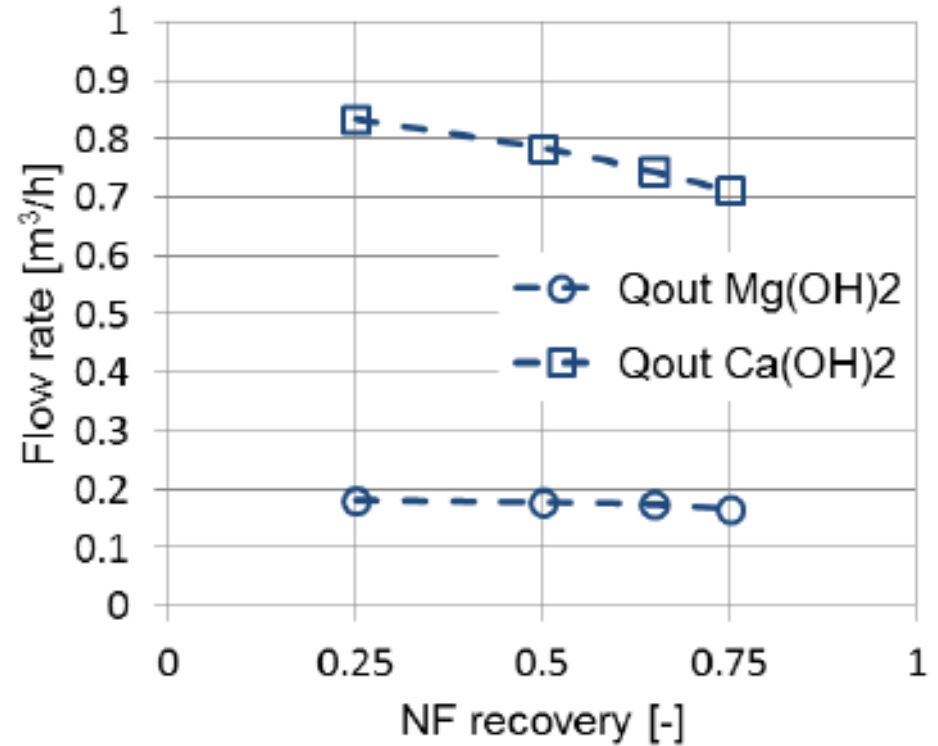
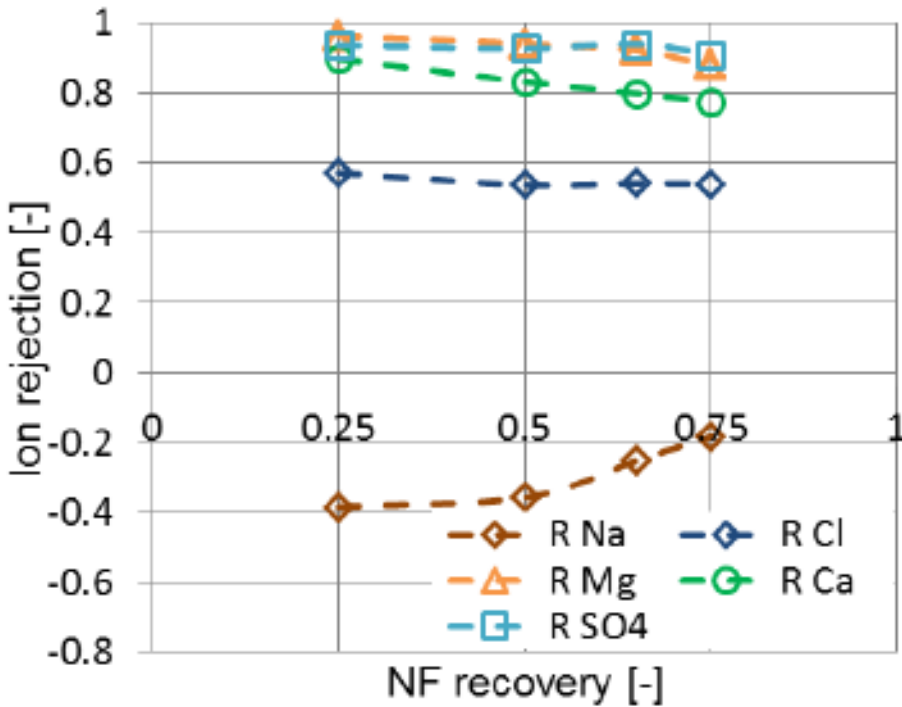
Input data still to be discussed and finalized

Crystallizer	$C_{NaOH}$ [M]	1
	S. excess Mg [%]	10
	S. excess Ca [%]	10
	$v_{feed}$ [cm/s]	4
	L [m]	2.3
MED (plane)	N [-]	13
	$P_{steam}$ [bar]	1
	$T_s$ [°C]	100
	$T_N$ [°C]	38
	Heat cost [\$/MWh <sub>th</sub> ]	<b>10</b>

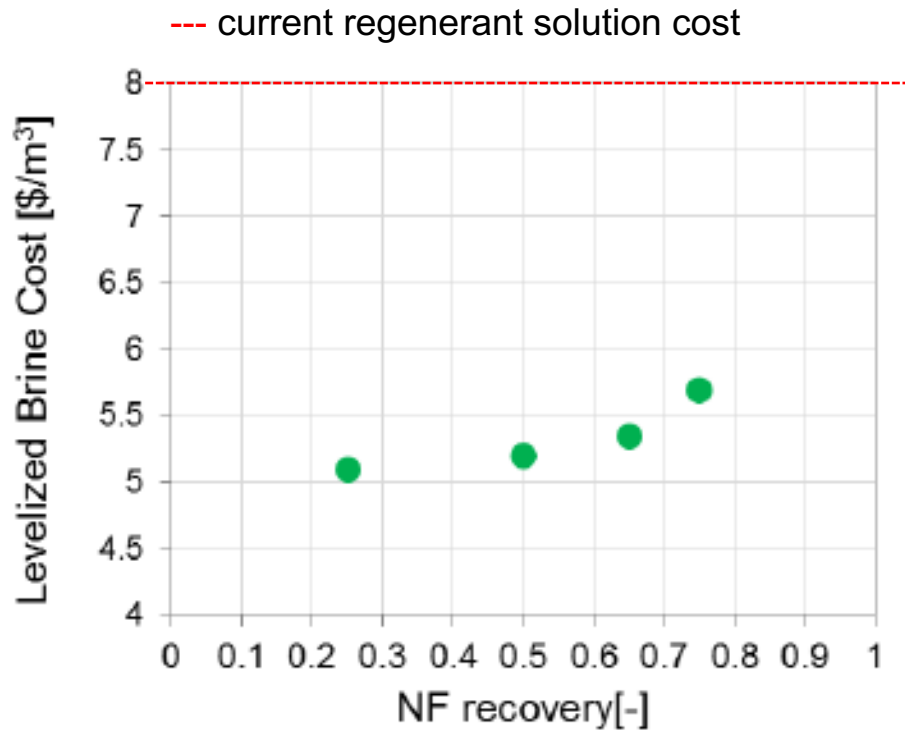




# Nanofiltration recovery variation: preliminary results



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**LBC<sub>tot</sub> ~ 5 \$/m<sup>3</sup> with R=25%**

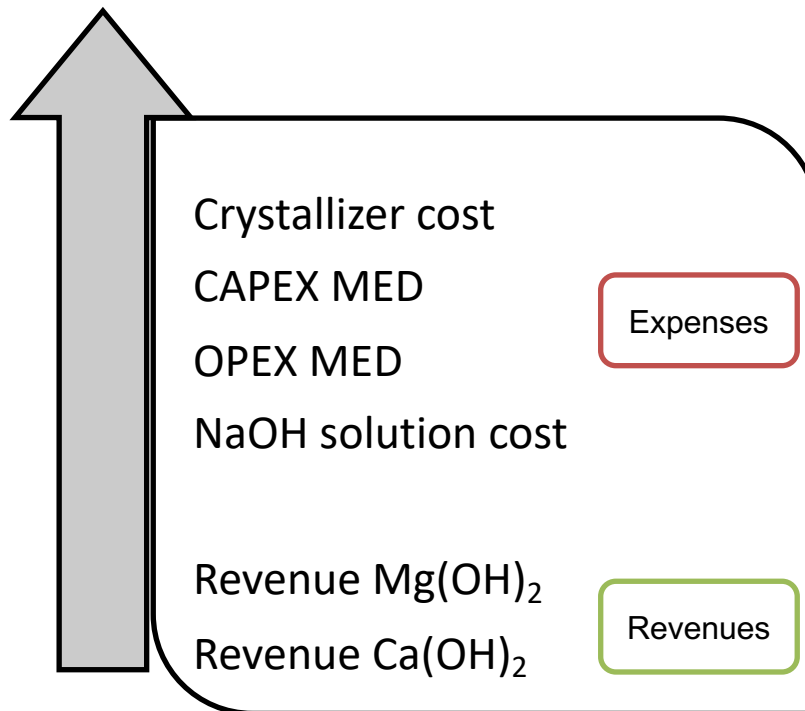
Current cost of regenerant = 8 \$/m<sup>3</sup>

Dependency on NF  
membrane properties



## Edge case: chain without NF (preliminary results)

- Presence of NaCl is not problematic in the crystallizer
- Lower concentrations of bivalent ions are favorable in the crystallizer (not too high supersaturation)

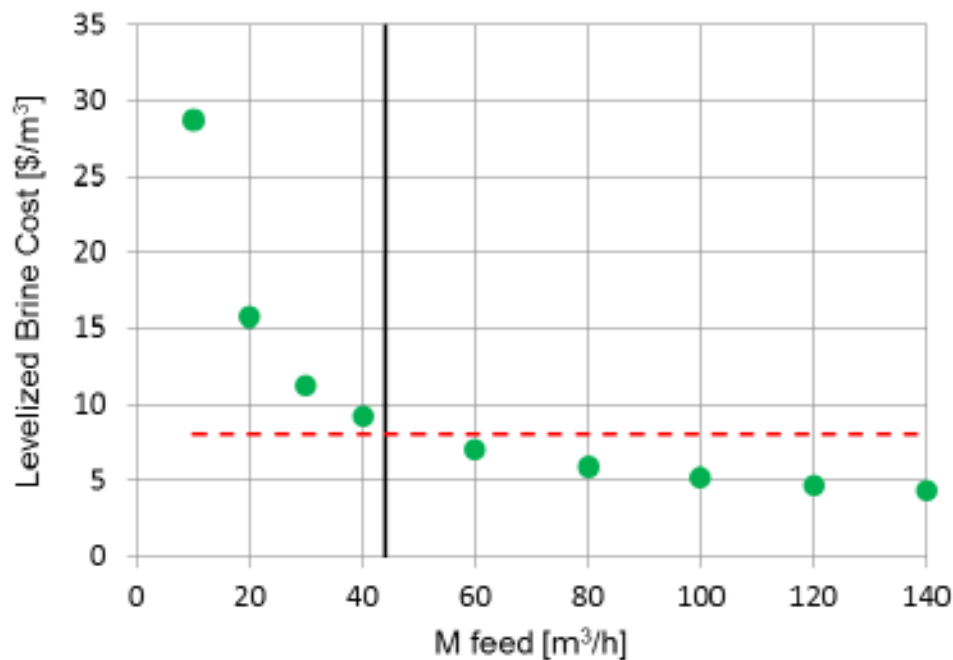


$LBC_{tot} = 3.9 \text{ \$/m}^3 < LBC_{tot}$  for the full chain with R=25%



# Feed flow rate variation: preliminary results

--- current regenerant solution cost



Flow rate produced in the Evides Site I?

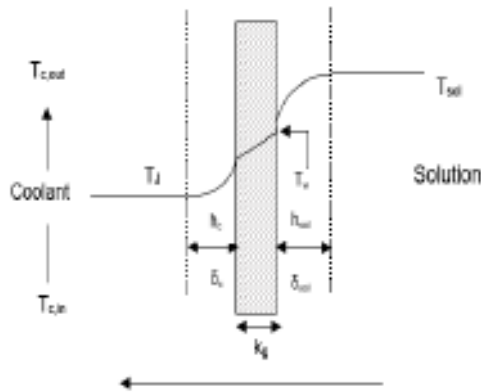
If 1060 m<sup>3</sup>/day ~ **45 m<sup>3</sup>/h**:

- LBC ~ 8.7 \$/m<sup>3</sup>
- without NF ~ 6 \$/m<sup>3</sup>

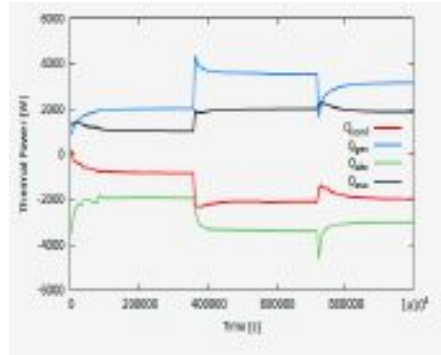




# Subtask 5.3 – EFC Model



Temperature profile across the subcooled heat exchanger surface.  $T_j$  is the average coolant temperature inside the jacket and  $T_{sol}$  is the average temperature of bulk solution in the crystallizer.



Example of a variation of thermal power delivered in function of operational conditions

✓ Multiple criteria evaluation and determination of the optimal operating strategy, studying:

- Energy consumption
- Operating costs
- CO<sub>2</sub> eq emissions
- ....

- ✓ Driving temperature variation (desorber)
- ✓ Sink temperature variation
- ✓ Variable cooling demand
- ✓ Operational constraints: impurity, crystal growth, etc.

